1	SELENIUM REMOVAL METHOD
2	
3	FIELD OF THE INVENTION
4	
5	The present invention relates to a method for removing selenium from
6	aqueous streams. More specifically, the present invention relates to a method
7	for removing selenium from wastewater effluent, and still more specifically, to
8	a method for removing selenium from petroleum refining wastewater. The
9	method is especially useful for removing selenium from streams from refinery
10	sour water strippers.
11	
12	BACKGROUND OF THE INVENTION
13	
14	Selenium is a naturally occurring element that can occur in several oxidation
15	states. It can exist in the [-II] (selenide), [O] (elemental selenium),
16	[+IV] (selenite), and [+VI] (selenate) oxidation states. Selenium can be
17	stabilized in aqueous solutions with CN to form selenocyanate or by organic
18	compounds to form mercaptan analogues such as dimethylselenide or
19	isoselenocyanates. Selenium is a ubiquitous element having an average
20	concentration of about 0.7 ppm in the earth's crust, and is concentrated in
21	such diverse things as plants, sulfur deposits, sulfide minerals of copper and
22	molybdenum, and fossil fuels. As a result, selenium can be found in waste
23	streams from copper refining, acid coal mine drainage, coal-fired power
24	plants, and petroleum refining. Selenium is generally considered to be
25	hazardous, and selenium disposal is carefully regulated.
26	
27	Selenium has also been found in waste agricultural irrigation water. In this
28	regard, the presence of selenium in waste agriculture and irrigation water
29	recently has become a major pollution concern. Selenium poisoning has been
30	implicated in waterfowl deaths and deformities at the
31	Kesterson National Wildlife, Refuge near Los Banos, California. The potential
32	of selenium poisoning, therefore, has generated significant interest in a

number of different industries where research activity has been directed to the removal of selenium from wastewater.

2

4

5

6

7

8

9

10

11

12

13

14

15

16

17

18

19

20

21

22

23

24

1

A particularly acute problem of concentrated selenium discharge occurs in the waste waters from petroleum refineries. Many refineries have this problem, to a lesser or greater extent depending on the origin of the crude oil. As the selenium is isomorphous with sulfur, it accompanies sulfur in the processing of the oil. If selenium is present it generally accompanies sulfur in the oil. Crude oil taken from the San Joaquin Valley in California, for example, has relatively high selenium content. Most of the sulfur and selenium found in crude ends up in refinery sour water streams which are subsequently treated by sour water strippers. However, while the stripping of hydrogen sulfide from sour water in conventional sour water strippers is highly efficient, significant amount of selenium compounds remains in the stripped sour water. The predominant selenium compounds remaining in the stripped sour water are hydrogen selenide and selenocyanate. Minor amounts of elemental selenium and oxidized forms such as selenite and selenate might also be present. Typically the stripped sour water, containing selenium compounds, is directed for further treatment with the rest of the refinery wastewater and in the process it gets oxidized to elemental selenium, selenite and selenates. As a result, in the waste water discharge from refineries processing crude oil high in selenium, selenium content has been high. In the case of several refineries located in the San Francisco Bay area the concentration of selenium in the wastewater could be above accepted levels for safe discharge.

2526

27

28

29

30

31

32

As noted above, selenium is introduced to the refinery process through the crude oil which is processed in the refinery. It may be partially removed in the initial crude dewatering and desalting steps, but much of the selenium is carried over into petroleum processing, such as hydroprocessing or fluid catalytic cracking. Selenium present in the products from these processes is removed by aqueous treatments such as washing and absorption. The aqueous streams from the various aqueous treatment processes in the

refinery are generally combined into a sour water stream, which is treated for 1 2 recycle and/or for disposal. 3 4 Sour water is process water recovered from petroleum or hydrocarbon 5 streams during refinery operations. For example, sour water may be 6 recovered from the petroleum streams, as in crude oil dewatering, it may be 7 recovered from a washing process, such as during crude oil desalting, or it 8 may be recovered from an absorption process, such as, for example, 9 removing sulfur and nitrogen compounds from hydroprocessed products. Sour 10 water generally contains soluble oil and free oil contaminants, inorganic ions 11 such as ammonia, sodium, sulfates, sulfites, chlorides, CO₂, OH and also solids that are typically corrosion products such as iron sulfides, iron oxides or 12 13 hydrates etc. 14 15 Sour water is typically processed in a sour gas stripper. A sour gas stripper is 16 a single or multi-stage separation zone for treating sour water. The stripping 17 action may be facilitated by the introduction of a hot gaseous stripping 18 medium, such as steam. The overhead stream from the sour gas stripper may 19 include ammonia, hydrogen sulfide, purified water vapor, or combinations 20 thereof, depending on the particular process. The bottoms product from the 21 stripper is a stripped sour water stream. The stripped sour water stream 22 generally contains the majority of the selenium compounds. Efforts to remove 23 the selenium from a sour water stream were unsuccessful so far. Effluents of 24 sour water strippers are difficult to treat for selenium removal because of the 25 unpredictable nature and unpredictable quantities of contaminants that are 26 present in the effluents. These contaminants often hinder irreversibly 27 selenium removal processes that use membrane, ion exchange resins or 28 inorganic adsorbents. The method of the present invention is especially useful for removing selenium from sour water in the presence of contaminants of 29

variable composition and quantity, especially in the presence of free and

soluble oil. However, any aqueous stream may be usefully treated using the

30

31

32

present method.

Because the selenium concentration in a typical refinery wastewater effluent 1 2 is generally very low, i.e., typically in the ppb range, wastewater treatment 3 techniques that have been used to remove selenium have been of the 4 adsorption type such as iron and aluminum hydroxide adsorption. Also, reverse osmosis techniques have been attempted and were found to be very 5 6 costly and difficult to operate due to membrane fouling with free oil and solids. The success of the various adsorption methods depends largely on the 7 8 selenium species present and on competitive ions in solution. 9 10 As noted above, selenium can exist as selenide, elemental selenium, selenite, 11 selenate, and selenium complexes with cyanite or organic bases. Of these 12 species, ion exchange favors selenocyanate over selenate and selenate over 13 selenite, whereas the iron hydroxide adsorption has no affinity for 14 selenocyanate and favors selenite over selenate. Since most refinery final 15 effluents and natural waters include a mixture of selenate and selenite 16 selenium species, it has been difficult to approach complete removal of 17 selenium from refinery effluents or natural water using only one step. 18 Furthermore, oxidation to, or reduction from, the selenate state is kinetically 19 very slow which further inhibits optimization. Ion exchange also has not been 20 a successful removal technique because selenate shows almost identical 21 resin affinity as sulfate, which is usually present in a concentration of several 22 orders of magnitude higher than selenate. Thus, the sulfate simply 23 preferentially competes with selenium for resin sites. Furthermore, ion 24 exchange resins become fouled when used to treat selenium wastewater and 25 methods for regeneration are often inadequate and unpredictable. 26 27 Among other things, the method of the present invention quantitatively, and 28 inexpensively, removes selenium from stripped sour water prior to combining 29 the stripped sour water with other refinery wastewater for further processing. 30 31 As noted previously, the method of the present invention is especially 32 effective with respect to the removal of selenium from the strip sour water 33 effluent waste waters produced from petroleum refineries, although it is useful

with other industrial effluent waters as well. Industrial processes include 1 2 synfuel from coal conversion and many metallurgical processes, particularly precious metals process solutions that involve cyanidation of selenium 3 4 containing precious metal ores or concentrates. The latter includes mineral 5 processing waste, and particularly heap leach gold mine washings. In the 6 case of some industrial processes there will also be, or there will alternatively 7 be, molybdenum and/or other toxic metals present. The method of the 8 invention is effective to remove most such toxic metals, as well as selenium. 9 10 Current methods for removing selenium from stripped sour water involve ion 11 exchange resin. In these methods, the selenium-containing sour water passes 12 over an ion exchange resin, which selectively adsorbs the selenium. While 13 this method is effective, ion exchange resins are very expensive. Further, their 14 use in this service is severely limited by the tenacity with which selenium, 15 particularly selenocyanate, irreversibly adsorbs on the ion exchange resin. 16 Methods for removing the selenium and regenerating the resin are generally 17 ineffective, thus rendering the resin permanently deactivated. The present 18 invention provides, among other things, a way to quantitatively remove the 19 selenium from stripped sour water in a cost effective manner by passing a 20 selenium-containing aqueous stream in combination with a quaternary amine 21 compound through a filter and recovering a treated aqueous stream which is 22 depleted in selenium content relative to the untreated selenium-containing 23 aqueous stream. 24 25 An example of an ion exchange process is disclosed in 26 U.S. Patent No. 4,915,928 to Marcantonio. The patent relates to a process for 27 removing selenium from wastewater effluent which includes the steps of; 28 (i) contacting a selenide containing wastewater and a strong-base anion 29 exchange resin to absorb selenide on the resin; (ii) eluting the ion exchange 30 resin with an eluant which is effective for stripping selenide therefrom; and 31 (iii) recovering elemental selenium from the selenide containing eluate 32 resulting from step (ii).

1 A process for removing selenium, present in the waters as selenocyanate, by 2 precipitation with copper (II) salts was shown to effectively precipitate 3 selenium under laboratory conditions. In this process the selenium is 4 precipitated as an alpha Cu(S0.91Se0.09)CN solid solution. However, this 5 process, although successful under controlled conditions did not work well in 6 an actual refinery operation. 7 8 There is a need for a reliable process for removing selenium from refinery wastewaters under actual refinery operating conditions where the amount of 9 10 free oil contaminants and soluble oil contaminants vary unpredictably. The 11 present invention, among other factors, provides such a process. 12 13 SUMMARY OF THE INVENTION 14 15 The present invention provides a method for removing selenium from an 16 aqueous stream by passing the aqueous stream, in combination with a 17 quaternary amine compound, through a filter and recovering a treated 18 aqueous stream which is depleted in selenium content relative to the 19 untreated agueous stream. The present method removes selenium from an 20 aqueous refinery stream by passing the aqueous stream, in combination with 21 a quaternary amine compound, through a filter that can include clay, cellulose, 22 starch, activated carbon, and the like. 23 24 <u>Detailed Description</u> 25 26 As discussed in detail in the "Background of the Invention", selenium is 27 introduced to the refinery processes through the crude oil. Selenium present 28 in the products from these refinery processes is removed by aqueous 29 treatments and combined into sour water streams and steam stripped before 30 reuse or ultimate disposal. And because selenium is frequently regulated by

refinery NPDES permits, it must be removed from the sour water streams

before they are discharged. As was also discussed, conventional ion

31

exchange methods for removing the selenium from stripped sour water are 1 2 very expensive. 3 4 While not being bound to any particular theory of operation, the present 5 method is based in part on the discovery that selenium compounds, especially 6 selenocyanate and free and soluble oil co-adsorb strongly and irreversibly on 7 conventional filter materials in the presence of quaternary amines. This 8 discovery is significant because at least a portion, and generally a major 9 portion, of the selenium in sour water occurs as selenocyanate (SeCN). Add 10 to this the fact that conventional filter materials such as clay, cellulose, starch, 11 activated carbon and the like are substantially cheaper than conventional 12 resins and therefore may be economically sent for disposal when saturated. 13 Clay especially, can operate at high temperature encountered in stripped sour water effluent streams (200°F - 300°F). So, the present invention 14 15 unexpectedly provides a method for removing selenium without plugging and 16 without fouling even when oil or other fouling components are present. 17 18 The term "selenium" as used herein generally refers to all compounds of the 19 element selenium including for example selenite and selenate, as well as the 20 elemental form. 21 22 The filter used in the method of the invention includes filter media which will 23 absorb or otherwise remove a quaternary amine compound from an aqueous 24 solution. Examples of filter media that may be used in practicing the invention 25 include clay, cellulose, starch, activated carbon, and the like. Other filter 26 media may be used that will be apparent to those persons having ordinary 27 skill in wastewater treatment technology. 28 29 Filters suitable for practicing the present method are available commercially. 30 These filters contain a filter medium containing a quaternary amine in 31 combination a solid sorbent. These are marketed for the purpose of removing 32 oil from aqueous streams, and are generally used during crude oil production, 33

particularly on oil platforms. Using filters that contain a quaternary amine

1 compound eliminates the need to add the compound to the 2 selenium-containing aqueous solution and as a consequence is a preferred embodiment of the invention. These quaternary amine-containing filters are 3 4 available from the following companies: 5 6 CETCO - clay filter medium 7 Clerity and US Filter/Ametek - cellulose medium 8 Clearwater - starch medium 9 10 Quaternary amine compounds are synthetic derivatives of ammonium 11 compounds, generally ammonium chloride, with the generalized formula R¹ R² R³ R⁴ N+ X-, where R¹ R² R³ and R⁴ are the same or different and are an 12 alkyl or aryl group, preferably an alkyl group, more preferably linear and 13 14 branched paraffins having a chain length of C₄ - C₆, preferably C₄ - C₂₀, and more preferably C_4 - C_{12} and X is an anion (e.g. halogen, such as bromide, 15 16 iodide, or chloride). 17 Quaternary amines have been used to remove oil and water soluble organics 18 19 from water as disclosed in U.S. Patent Nos. 5,354,477 and 6,159,379, 20 incorporated by reference herein. Use of CrudeSorb® to remove oil from 21 produced water is described in "Produced Water Polishing" 22 CETCO Offshore - Technology Paper (December 2002). 23 24 Although using a filter medium that contains a quaternary amine compound is 25 a preferred embodiment of the present method, a filter medium that does not 26 contain a quaternary amine compound may suitably employed. In this case, a 27 quaternary amine compound is added to the wastewater. 28 29 The present method is quite flexible in its application and may be practiced 30 under a wide variety of conditions. Optimization of these conditions is within 31 the purview of a person having ordinary skill in wastewater treatment

32

technology.

The temperature at which the aqueous stream containing selenium may be 1 2 treated is not critical and generally ranges from ambient temperature up to the boiling temperature of the aqueous stream. Temperatures lower than ambient 3 4 temperature may also be used. 5 6 Likewise, the pressure at which the aqueous stream containing selenium may 7 be treated is not critical and generally ranges from ambient pressure up to 8 about 200 psig. The flow rate of the aqueous stream depends on the 9 particular processing equipment that is employed and could range from 0.1 to 480 gpm and in practice will typically range from 48 to 480 gpm. 10 11 12 A prefiltration step may be used in carrying out the method of the present 13 invention. For example, sock filtration may be used before the main filtration 14 units to act as a prefiltration to capture particulates and prevent them from 15 impacting the main filtration units. Were such particulates to escape that could 16 result in premature fouling or plugging of the main filtration units. Other 17 methods of prefiltration of wastewater are well known and could be used. 18 19 The effluent stream from the filter may be monitored to ensure complete 20 selenium removal. Selenium breakthrough conditions as determining by 21 measuring selenium concentration in the wastewater treated by the filter 22 would typically indicate that the filter is saturated and must be replaced. The 23 filter is then generally sent for disposal or special regeneration. 24 25 In another embodiment of the present invention, the selenium removal is 26 conducted in two stages. In this embodiment, after passing the aqueous 27 stream in combination with a quaternary amine compound through a filter to 28 produce an effluent which is depleted in selenium content relative to the 29 untreated selenium-containing aqueous stream, the effluent is passed through 30 a conventional filter medium, preferably activated carbon, whereby the 31 effluent is further depleted in selenium content.

W .

In yet another embodiment of the present invention, the selenium removal is 1 2 conducted in multiple stages. In this embodiment, after passing the aqueous 3 stream in combination with a quaternary amine compound through a filter to 4 produce an effluent which is depleted in selenium content relative to the 5 untreated selenium-containing aqueous stream, the effluent is passed through 6 a conventional filter medium, preferably activated carbon, whereby the 7 effluent is further depleted in selenium content. The treated effluent is then 8 contacted by an anion exchange resin in one or more columns as described, for example, in U.S. Patent Nos. 4,915,928 and 5,601,721, which are 9 10 incorporated by reference as if fully set forth herein. The method of the 11 present invention is especially advantageous in this embodiment because the 12 resin is contacted with only minimal amounts of selenium and will 13 consequently have a much longer run life than when an ion exchange resin is 14 used alone.

15 16

و الأ

<u>EXAMPLES</u>

17 18

The following examples are intended to illustrate the present invention and are not intended to limit the invention in any way.

192021

Materials:

2223

24

25

26

27

28

2930

31

32

33

Stripped sour wastewater was obtained from an oil refinery. The wastewater contained selenium produced from the refining of crude oil. A portable diesel driven centrifugal pump was used to move the selenium containing wastewater through the train of filters. The pump had a maximum capacity of 40 gallons of water per minute was used to feed the wastewater through the pilot plant filtration system. The pilot plant filtration system was comprised of at least one CETCO filtration unit containing twenty four CrudeSorb® filter canisters or approximately twelve cubic feet of CrudeSorb® media. The pilot plant filtration system also contained at least one activated carbon unit containing approximately twelve cubic feet of Calgon activated carbon, a mixture of F₃₀₀ and F₄₀₀ activated carbon. The pilot plant filtration system also

1 consisted of at least two resin filtration units each containing approximately 2 twelve cubic feet of anion exchange resin (Sybron Ionac). 3 4 **Experiment**: 5 6 The method of the present invention was demonstrated in a pilot plant 7 filtration system with four filtration units. In addition, sock filtration was used in front of the four main filtration units to act as a prefiltration. The first filtration 8 9 unit of the pilot plant filtration system was designed using the 10 CETCO CrudeSorb® for the initial purpose of reducing the oil and 11 grease levels in the waste water and preventing the fouling of the 12 subsequent filtration units by oil and grease. The CrudeSorb® not 13 only absorbed oil and grease as expected but surprisingly absorbed 14 much more selenium than expected. The next filtration unit was filled 15 with activated carbon. This was followed by two anion exchange resin 16 filled filtration units to reduce the concentration of RCRA hazardous metals 17 such as selenium. 18 19 The pilot plant filtration system contained prefiltration consisting of two sock 20 filters. The prefiltration was followed by a CETCO filtration unit containing 21 (24) CrudeSorb® filter canisters, an activated carbon filtration unit containing 22 twelve cubic feet of Calgon activated carbon, and two resin filtration units 23 each containing twelve cubic feet of anion resin. Each filtration unit was 24 connected in series from top inlet to bottom discharge. Water samples were 25 taken at the storage tanks before the start of each pilot run and at each 26 filtration unit outlet at four hour intervals for up to 36 hours. Water sampling 27 was conducted in compliance with refinery SOP and quality assurance 28 protocols as well as USEPA sampling protocol. A diesel powered centrifugal 29 pump was used to push the waste water through the pilot plant filtration 30 system at feed rates up to 28 gpm and as low as 13gpm. Selenium levels

were measured using USEPA Method 200.7 or APHA 3114B.

1 The pilot plant filtration system was operated at ambient temperature, but was 2 capable of running at temperatures up to the boiling point of the aqueous 3 stream. The pressure was less than 100 psig. The flow rates can range from 4 0.1 to 40 gpm depending on the particular processing equipment. The effluent stream from the filter outlets was monitored to ensure selenium removal and 5 6 to indicate selenium breakthrough once the filter was saturated. 7 8 **Results and Discussion:** 9 Some reductions in selenium levels were expected in the carbon filtration unit 10 and more so in the two anion resin units. However, it was found that the 11 CETCO filtration unit containing CrudeSorb® filter canisters, which contain a 12 13 quaternary amine compound, was surprisingly very effective at removing the 14 selenium contained in the stripped sour water. 15 The first pilot plant run (Table 1) lasted 32 hours indicating that the 16 17 CrudeSorb® removed the selenium at an averaged rate of 74% with the 18 activated carbon removing the remaining selenium to a non detection limit of 19 less than 2 µg/liter. The feed rate was 25 gpm with a total waste water volume

treated of 50,148 gallons. The feed initial selenium level composited was

20

21

161 µg/l.

1 <u>TABLE 1</u>

2

Run 1 Run					
Time	Feed	QA	Carbon	Resin 1	Resin 2
0	126	0	0	0	0
4	130	46.5	20.7	0	0
8	124	63.6	46.4	0	0
12	83	10.4	0	0	0
16	115	10.1	0	0	0
20	147	0	0	0	0
24	111	49.9	19.7	0	0
28	165	78.6	55.3	0	0
32	200	57.6	47.5	15.1	0

Feed Rate = 25 GPM Volume = 50,148 gallons pH = 8.11 Initial Se = 161 ug/l

Amount of Removal µg/I

Run	1-3			
Time	QA	Carbon	Resin 1	Resin 2
0	126	0	0	0
4	83.5	25.8	20.7	0
8	60.4	17.2	46.4	0
12	72.6	10.4	0	0
16	104.9	10.1	0	0
20	147	0	0	0
24	61.1	30.2	19.7	0
28	86.4	23.3	55.3	0
32	142.4	10.1	32.4	15.1

3

- 5 A second pilot plant run (Table 2) using the same filtration system without
- 6 changing any of the filtration media was conducted for another 28 hours. The
- 7 feed rate was 25 gpm with a total waste water volume treated of
- 8 48,846 gallons. The feed initial selenium levels ranged from 776 to 843 μ g/l.
- 9 The CrudeSorb® removed the selenium at an averaged rate of 57% with the
- 10 activated carbon removing another 13% and the anion exchange resin
- 11 removing another 20%.

1 TABLE 2

2

Run 2				
Run Time	Feed	QA	Carbon	Resin 1
0	376	143	114	72.5
4	388	154	116	79.6
8	370	130	104	81.8
12	430	93.1	50.3	31.2
16	136.2	46.45	23.91	12.06
20	139.4	84.34	42.22	18.09
24	160.6	91.14	74.09	45.39
28	167.4	97.73	76.73	51.31

Feed Rate = 25 GPM Volume = 48846 gallons pH = 8.46 - 8.71 Initial Se = 776 - 843 μ g/l

Amount of Removal

	µg/i			
Run				
Time	QA	Carbon	Resin 1	Resin 2
0	233	29	41.5	57.9
4	234	38	36.4	38.9
8	240	26	22.2	34.7
12	336.9	42.8	19.1	21.1
16	89.75	22.54	11.85	12.06
20	55.06	42.12	24.13	18.09
24	69.46	17.05	28.7	17.5
28	69.67	21	25.42	9.81

- 5 A third pilot plant run (Table 3) using the same filtration system without
- 6 changing any of the filtration media was conducted for another 20 hours. The
- 7 feed rate was 28 gpm with a total waste water volume treated of
- 8 48,762 gallons. The feed initial selenium levels ranged from 130 to 190 μ g/l.
- 9 The CrudeSorb® removed the selenium at an averaged rate of 33% with the

- 1 activated carbon removing another 14% and the anion exchange resin
- 2 removing another 20%.

3 <u>TABLE 3</u>

4

Run 3 Run Time	Feed	QA	Carbon	Resin 1	Resin 2
		•			
0	158	111	84.1	55.5	42.5
4	154	92.8	80.1	51.6	50.8
8	134	98.6	89.5	64.2	60.4
12	152	107	69.6	57.8	52.2
16	195	122	105	86	75.6
20	182	121	76.3	83.2	109

Feed Rate = 28 GPM Volume = 48762 gallons pH = 6.79 - 7.36 Initial Se = 130- 190 μ g/l

Rate of Removal µg/l

	μθ/ι			
Run				
Time	QA	Carbon	Resin 1	Resin 2
0	47	26.9	28.6	13
4	61.2	12.7	28.5	8.0
8	35.4	9.1	25.3	3.8
12	45	37.4	11.8	5.6
16	73	17	19	10.4
20	61	44.7	-6.9	-25.8

5

- 7 A fourth pilot plant run (Table 4) using the same filtration system without
- 8 changing any of the filtration media was conducted for another 24 hours. The
- 9 feed rate was 28 gpm with a total waste water volume treated of
- 10 47,103 gallons. The feed initial selenium levels ranged from 204 to 246 μg/l.
- 11 The CrudeSorb® removed the selenium at an averaged rate of 36% with the

- activated carbon removing another 20% and the anion exchange resin
 removing another 25%.
- 3

TABLE 4

5

Run 4 Run					
Time	Feed	QA	Carbon	Resin 1	Resin 2
0	158	98.7	91	61.8	35.8
4	144	92.4	86.9	57.6	38.2
8	166	90.3	83.4	48.7	33.8
12	196	143	128	104	87.2
16	258	150	117	92.8	84.9
20	154	101	58.1	51.3	42.5
24	167	122	69.3	63.7	47

Feed Rate = 28 GPM Volume = 47103 gallons pH = 8.06 - 8.66 Initial Se = 204- 246 μ g/l

Amount of Removal

	μg/i			
Run	•			
Time	QA	Carbon	Resin 1	Resin 2
0	59.3	7.7	29.2	26
4	51.6	5.5	29.3	19.4
8	75.7	6.9	34.7	14.9
12	53	15	24	16.8
16	108	33	24.2	7.9
20	53	42.9	6.8	8.8
24	45	52.7	5.6	16.7

- 8 A fifth pilot plant run (Table 5) using the same filtration system without
- 9 changing any of the filtration media was conducted for another 56 hours. The
- 10 feed rate was 13 gpm with a total waste water volume treated of
- 11 51,786 gallons. The feed initial selenium levels ranged from 109 to 182 ppb.

The Crudesorb® was bypassed with the activated carbon removing 85% and 1 2 the anion exchange resin removing another 5%. 3 4 This last result was achieved with activated carbon alone and is a very good and guite unexpected result. This suggests that the composition of the 5 6 wastewater and especially of selenium compounds changed to the point 7 where activated carbon is also a very effective remover of selenium, just by 8 itself. This shows that having all three units operate in combination, a 9 quaternary amine filter, an activated carbon filter and an ion exchange is most 10 preferred embodiment, since the combination can handle variations in wastewater and still remove selenium to required levels. 11 12 13 The pilot tests results were surprising since they broke out of the predicted 14 ranges for both the quaternary amine and the activated carbon. This suggests 15 that something unpredictable is happening. Without being bound to any 16 particular theory of operation, a possible explanation could be that the composition of the stripped sour water changes all the time and there are 17 18 times that a quaternary amine works well; and sometimes the activated 19 carbon works well.

1 <u>TABLE 5</u>

2

Run 5 Run				
Time	Feed	Carbon	Resin 1	Resin 2
0	117	36.5	0	0
4	107	25	0	0
8	120	18.5	0	0
12	121	18.5	0	0
16	132	25.1	0	3.4
20	182	38.8	8.5	5.4
24	146	24.3	6.7	4.4
28	161	23.9	4.2	2.8
32	181	26.5	4.6	2.7
36	157	22.8	8.7	5.1
40	146	10.5	4.6	2.9
44	109	0	0	0
48	118	0	0	0
52	106	0	0	0
56	125	0	0	0

Feed Rate = 13 GPM Volume = 51786 gallons pH = 6.97 - 7.01 Initial Se = 189- 203 μ g/l

Amount of Removal µg/l

Carbon	Resin 1	Resin 2
80.5	36.5	0
82	25	0
101.5	18.5	0
102.5	18.5	0
106.9	25.1	-3.4
143.2	30.3	3.1
121.7	17.6	2.3
137.1	19.7	1.4
154.5	21.9	1.9
134.2	14.1	3.6
135.5	5.9	1.7
109	0	0
118	0	0
106	0	0
125	0	0
	80.5 82 101.5 102.5 106.9 143.2 121.7 137.1 154.5 134.2 135.5 109 118	80.5 36.5 82 25 101.5 18.5 102.5 18.5 106.9 25.1 143.2 30.3 121.7 17.6 137.1 19.7 154.5 21.9 134.2 14.1 135.5 5.9 109 0 118 0 106 0

- 1 Although the present invention has been described in detail with reference to
- 2 some preferred versions and examples, there are numerous variations on the
- 3 present invention which are possible in light of the teachings and supporting
- 4 examples described herein. It is therefore understood that within the scope of
- 5 the following claims, the invention may be practiced otherwise than as
- 6 specifically described or exemplified herein.